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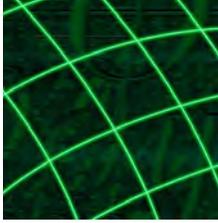


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**SPECIAL
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Objectives



The **International Journal of Computational Methods and Experimental Measurements (CMEM)** provides the scientific community with a forum to present the interaction between the complementary aspects of computational methods and experimental measurements, and to stress the importance of their harmonious development and integration.

The steady progress in the efficiency of computers and software has resulted in the continuous development of computer simulation, which has influenced all scientific and engineering activities. As these simulations expand and improve, the need to validate them grows, and this can only be successfully achieved by performing dedicated experimental tests. Furthermore, because of their continual development, experimental techniques are becoming so complex and sophisticated that they need to be controlled by computers, with the data obtained processed by means of computational methods.

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PREFACE

The contents of this issue reflect the rapid advances that have taken place in materials science and engineering, prompted by the demand for high quality performance materials by industry.

The contributions represent some of the latest developments in the field of Materials Characterisation, describing procedures for the assessment of physical and chemical properties of materials by experimental and computational methods. Apart from microstructural and macro-mechanical investigations on metallic substances, extensive coverage is also given to composites, biomaterials, polymers, ceramics and cementitious materials as well as to the effectiveness of various surface treatments. The wide range of topics includes interaction between disciplines, which is sometimes essential to achieving a proper understanding of material behaviour.

All issues, including this one, have been published in paper as well as digital format and are being widely distributed throughout the world

The Editors
Tallinn, Estonia
2017

PREDICTIVE AND PROGNOSTIC MODELLING AND SIMULATION OF COATINGS SUBJECT TO CORROSION AND MECHANICAL FAILURES

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ABSTRACT

This research presents analytical and mathematical modelling of coating failures within industrial components, structures, mobile assets and systems due to corrosive degradation and mechanical fracture. These failures lead to several surface problems; therefore, contact mechanics and electrochemistry approaches incorporating induced residual stresses have been adopted to develop a comprehensive solution for the prediction and prognostic of such failures. Experimental study of film cracking and its propagation into substrates, interfacial transient behaviours and film-substrate system has been conducted. A parallel study of corrosive degradation to include cathodic delamination, cathodic blistering and tribo-corrosion of films has been conducted. Experimental and analytical studies of induced residual stresses within the coating and their effects on failure mechanisms and propagation have been completed. A detailed investigation of elastic mismatch at the interfacial contact and interfacial crack tip field has been performed and a complex stress intensity factor is presented. Mathematical derivation of oscillatory singularity, mode mix and interfacial fracture criterion to include adhesion are presented. This paper presents novel mathematical modelling incorporating interfacial crack propagating, diffusion of corrosive species and cathodic blistering for prediction and prognoses of coating failures.

Keywords: coating failure, compressive residual stress, diffusion induced stress.

1 INTRODUCTION

Protective coatings on industrial components and structures act as a barrier to preserve them from chemical and physical attack. Various environmental and mechanical factors are involved in the breakdown of coating on metallic surfaces. Defects in coating and substrate are formed during the fabrication process and during the application of system. The difference in coefficient of thermal expansion between coating and the substrate is the major cause of producing micro-cracks in coating. Cracks can also occur due to abrasion, physical or mechanical contact. The presence of residual stresses in coating and substrate system causes compressive and tensile stress. In corrosive environment, tensile residual stress results in crack opening, which leads to stress corrosion cracking. Micro-cracks provide passageway to corrosive species to diffuse into substrate and cause electrochemical reactions which results in coating delamination [1]. However, compressive residual stress closes the micro-cracks, but it causes the blister delamination when these stresses are sufficiently high [2]. Compressive residual stress and diffusion induced stress play a major role in adhesion loss of coating from the substrate. Various mathematical models have been formulated to model these two parameters for reliability assessment. Current work presents predictive modelling for the propagation of coating deformation in the presence of micro-cracks as a function of compressive residual and diffusion induced stresses.

2 BACKGROUND

A model for de-bonding driving force as a function of stress to predict the duration of useful life of isotropic coatings is presented in [2]. Elastic modulus and residual stress play a major role in the formation and propagation of blisters [3]. Stress-driven viscoplastic deformation conditions were also proposed to explain blistering mechanism [4]. Modified model to explain the deformation induced by residual stress for multilayer structure has been proposed in [5]. Later on, closed form solutions have been proposed in [6–8] by incorporating residual stress parameter. Diffusion induced stress factor is also a major cause for coating delamination, which cannot be neglected and has drawn considerable interest of researchers in the past decade. Various mathematical models have been proposed to model the concentration and diffusion of corrosive species inducing stress in the system. The effects of diffusion stress has been investigated in [9]. A theory has been presented in [10] that describes the delamination initiation when ions migrate through conductive passages which are usually formed in the presence of water molecules in hydrophilic and low molecular weight regions. Prognostic model designed in [10] was a function of blister size, ion diffusivity, potential gradient and distance between defect and blister. Diffusion induced stress is also a major problem in lithium ion batteries. The surface energy has been modelled by merging diffusion induced stress problem [11]. Considering diffusion induced stress and residual stress as important delamination parameters, it is very important to investigate and model the coupling behaviour of both factors.

Nanocorr, Energy and Modelling (NCEM) research group has been investigating corrosion and coating failure problems in isotropic organic coatings. Various parameters have been investigated and modelled to explain the behaviour of corrosion and coating failures [12–25]. Recently, the coupling effects of compressive residual stress and diffusion induced stress have been investigated through experimental analysis to model the formation and propagation of circular blisters in the presence of micro-cracks over coated surface. In this research, the de-bonding driving forces for straight-sided blister are modelled to explain blister formation and propagation mechanism in the presence of micro-crack.

3 EXPERIMENTAL ANALYSIS

In order to analyse the effect of compressive residual stress and diffusion induced stress, corrosion test was applied on coated samples having micro-crack over coating [16]. Seven samples were used to obtain cross-sectional measurements. AISI-1020 carbon steel samples 0.18%–0.23% C, 0.3%–0.6% Mn with balanced Fe were used for experimental analysis as substrates. The thicknesses of samples were 0.01 cm with elastic modulus of 200 GPa and coefficient of thermal expansion as $11.7 \times 10^{-6} \text{ K}^{-1}$ [26]. Sample were polished with emery paper of grit size 200 then conditioned with distilled water and dried with cold air.

Spray gun was used to apply red oxide primer coating on samples. The elastic modulus of red-oxide is 6.14 GPa with coefficient of thermal expansion as $21.6 \times 10^{-6} \text{ K}^{-1}$. Coating thickness was 20 μm . Micro-cracks were induced over the coating surface with initial aperture size of 2.1 μm . Residual stresses were measured through charge coupled device (CCD) detector and laser optics, which measures stress by monitoring substrate curvature. When samples were exposed to corrosive environment and monitored through the microscope, it was observed that several blisters and micro-cracks started to appear over the surface of coated samples. All the micro-cracks have shown almost similar behaviour but single micro-crack from each sample is considered for cross-sectional observation and analysis which is a destructive method.

The purpose of experimental work was to analyse the effects of residual induced stress in presence of diffusion induced stress. Samples were kept at fabrication temperature of 318K then transported to corrosive atmospheric chamber for accelerated testing. The fog, 5 parts of NaCl in 95 parts of distilled water, was simulated. The samples were placed at 60°C to avoid any direct pathways of crystallisation into the coating. The corrosive atmosphere was accelerated by gradually increasing the temperature. The temperature was raised 1K for every one hour. Cross-sectional images of each sample were taken during the temperature values i.e. 319K, 321K, 328K, 333K, 353K. During microscopic analysis, temperature is maintained similar to that in the corrosion simulation chamber for precision. Diffusion induced stress was induced by the presence of corrosive species in the environmental chamber and residual stress was induced by the change in temperature due to elastic mismatch. Micro-cracks provide channels for the species to diffuse into the system. Tensile and compressive behaviour of residual stress controls the opening and closing of pre-existing micro-cracks in the coating. The experimental compressive residual stress and diffusion induced stress with respect to change in temperature are shown in Fig. 2. The investigation of micro-crack propagation is divided into three regions and the resultant stress for controlling blister propagation was derived.

Region 1:

The experiment was initiated from fabrication temperature (318K) of system and increased to 319K. The aperture size of micro-crack was measured to be 2.1 μm, as shown in Fig. 1(a), which provided channel for the corrosive species to diffuse into the system, as a result the

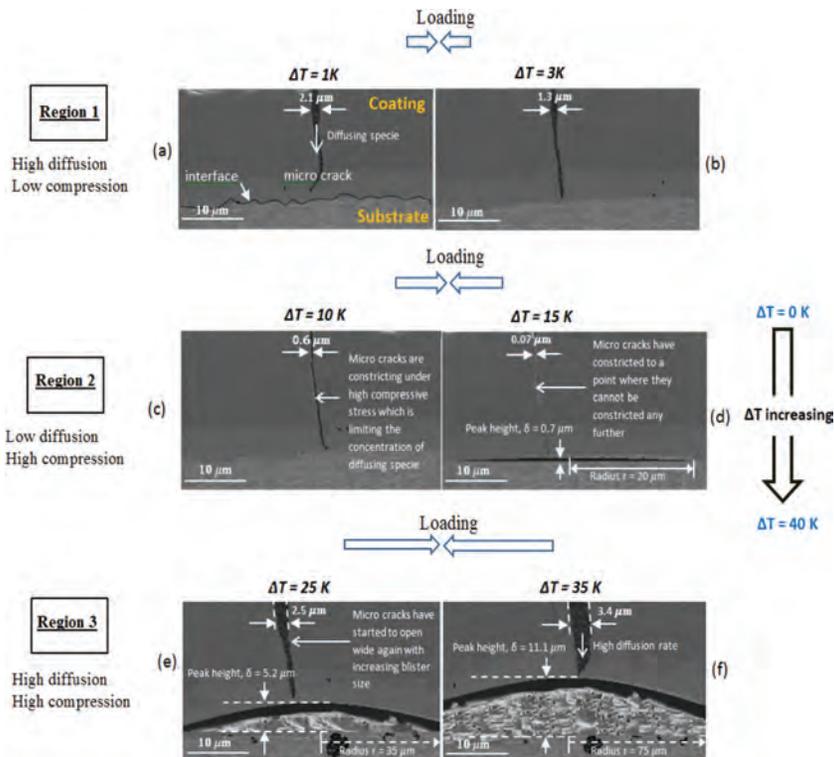


Figure 1: Samples micrographs at various temperature values [16].

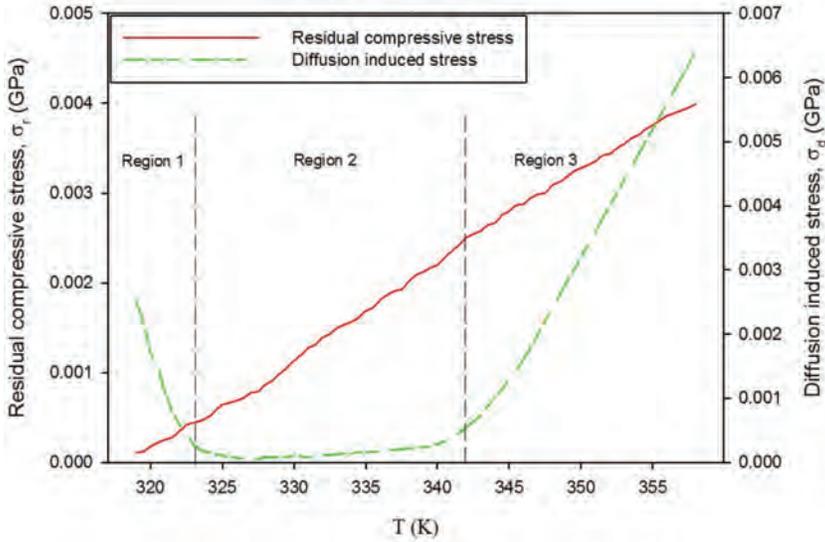


Figure 2: Experimental results of residual compressive stress and diffusion induced stress [16].

diffusion stress was high at the beginning of the experiment, as shown in Fig. 2. When the temperature is further increased to 321K the micro-crack started to shrink due to the rise in compressive residual stress but no major blistering effect was observed. The aperture of micro-crack decreased to $1.3 \mu\text{m}$, as shown in Fig. 1(b). Small decrease in diffusion induced stress was observed due to minor rise in temperature. Diffusion induced stress in this region appears to be a major controlling factor. According to the theory of linear superposition the following relation can be concluded.

$$\sigma = \sigma_r + \sigma_d \cong \sigma_d. \quad (1)$$

Region 2:

When the temperature was raised to 328K, the aperture size of micro-crack decreased to $0.6 \mu\text{m}$. The reason of this decrease in the size is the increase in compressive residual stress that can be seen in the results, which are plotted in Fig. 2. The compressive residual stress continued to increase from 0.004 GPa to 0.0023 GPa in region 2. The decrease in channel size for the corrosive species to diffuse into the system also decreased the diffusion induced stress. Further increase in the temperature to 331K, increased the compressive residual stress which reduced the aperture size to $0.07 \mu\text{m}$. This increase in compressive residual stress initiated the blistering effect, which can be seen in Fig. 1(d). Residual compressive stress can be considered as a significant influential parameter and can be written as:

$$\sigma = \sigma_r + \sigma_d \cong \sigma_r. \quad (2)$$

Region 3:

When the temperature was increased to 341K, compressive residual stress increased significantly which leads to blistering delamination. The size of the blister increased thus making the aperture size of micro-crack to further increase to $2.5 \mu\text{m}$. The widening of micro-crack provided more space for corrosive species to diffuse into the system, hence diffusion induced stress started to rise after 341K. In region 3, the behaviour of increase in compressive residual stress and diffusion induced stress was observed to be identical. The amplitude and radius of

blister as observed was 5.2 μm and 35 μm , which continually increased and reached up to a radius as 75 μm and amplitude as 11 μm . After applying the principle of linear superposition on coupling effect of compressive residual stress and diffusion induced stress for blister growth and propagation, the following relation can be derived as:

$$\sigma = \sigma_r - \sigma_d \tag{3}$$

The relation of compressive residual stress and diffusion induced stress proposed in eqn (3) is considered as a major controlling factor in blistering delamination mechanism. The coupling effect relation for compressive residual and diffusion induced stress has been previously incorporated for de-bonding driving force of circular blister growth and propagation. In current research the de-bonding driving force for straight-sided blister growth and propagation is proposed. Modelling of circular blister and straight-sided blister is derived in the next section.

4 MATHEMATICAL MODEL

The coupling effect of compressive residual stress and diffusion induced stress has been investigated through experimentation and the relation for stress as a function of compressive residual stress and diffusion induced stress has been proposed by using the principle of linear superposition theory. This paper discusses the incorporation of observed stress behaviour in circular blister propagation and based on that theory, relations for de-bonding force of straight-sided blisters are also proposed. Multi-disciplinary modelling approach has been adopted to explain the effect of stresses in coating delamination process. The designed and proposed models are based on the concepts of thermodynamics, mechanics and bi-layer cantilever beam theory. The critical stress level in the system can be calculated by using the following relation [2]:

$$\sigma_{cr} = 1.2235 \frac{E}{(1-\nu^2)} \left(\frac{h}{r}\right)^2 \tag{4}$$

Here, σ_{cr} is the critical stress, which computes critical threshold for the initiation of delamination, h is coating thickness, r is radius of blister, E is elastic modulus and ν poisson’s ratio. The coupling effect of compressive residual stress and diffusion induced stress controlling the transport of corrosive species as observed through experimental analysis [16] can be written as follows:

$$\sigma_0 = \frac{\partial \sigma_{r_c}}{\partial x} - \frac{\partial \sigma_{d_c}}{\partial t} \tag{5}$$

σ_0 represents total stress according to linear superposition theory, $\frac{\partial \sigma_{r_c}}{\partial t}$ is the change in compressive residual stress with respect to location x and $\frac{\partial \sigma_{d_c}}{\partial t}$ is the change in diffusion induced stress with respect to time t, change in concentration of corrosive species as a function of environmental parameters and the coupling effects of diffusion induced and compressive stress was derived [16] as:

$$\frac{\partial c_{k_c}}{\partial t} = \left\{ \begin{aligned} & \left(D_{k_c} + \frac{D_{k_c} E_c V_{k_c}^2}{9RT} c_{k_c} \right) \frac{\partial^2 c_{k_c}}{\partial x^2} + \frac{D_{k_c} E_c V_{k_c}^2}{9RT} \left(\frac{\partial c_{k_c}}{\partial t} \right)^2 - \\ & \frac{D_{k_c} E_c V_{k_c}^2}{9RT} \frac{\partial c_{k_c}}{\partial t} \left(\frac{\partial \sigma_{r_c}}{\partial x} - \frac{\partial \sigma_{d_c}}{\partial t} \right) \end{aligned} \right\} \tag{6}$$

$\frac{\partial c_{k_c}}{\partial t}$ represents a change in the concentration of corrosive species on coating and substrate system through micro-cracks, D_{k_c} diffusion coefficient of coating, T is temperature, R is molar gas constant and V_{k_c} is partial molar volume of coating material. Coupling effect of stress using eqn (2) can be written as:

$$\sigma_0 = \frac{\partial \sigma_{r_c}}{\partial x} - \frac{\partial \sigma_{d_c}}{\partial t} = \left(D_{k_c} + \frac{D_{k_c} E_c V_{p k_c}^2}{9RT} \right) \frac{\partial^2 c_{k_c}}{\partial x^2} + \frac{D_{k_c} E_c V_{p k_c}^2}{9RT} \left(\frac{\partial c_{k_c}}{\partial t} \right)^2 \left(\frac{D_{k_c} V_{p k_c}^2}{9RT} \frac{\partial c_{k_c}}{\partial t} \right)^{-1} \quad (7)$$

4.1 De-bonding driving force for circular blister

When coating remains intact with the substrate, there is no de-bonding driving force. The blistering effect appears when de-bonding driving force exceeds critical threshold value. The blisters shapes can be circular which end up in telephonic cord like shape and blister can also lead to straight-sided shape which ends up as snakes back forth shape [27]. In this research paper the coupling effect of compressive residual stress and diffusion induced stress, which was investigated for circular blister through experimental results, is incorporated for straight-sided blister to model de-bonding driving force [16]. First, the derivation of de-bonding driving force for circular blister is discussed and then, relations for straight-sided blisters are proposed. The model for circular blister is already analysed and validated through experiments while strain energy release rate for straight-sided blister has already been discussed and validated [16, 27]. So, new relations for straight side blister are based on two verified and validated theories. Strain energy release rate stored for circular blister can be written as:

$$G_0 = \frac{(1-\nu)h \sigma^2}{E} \quad (8)$$

Strain energy release rate for crack propagation derived in Ref. [2] is given as:

$$G = 6 \frac{(1-\nu^2)}{E h^3} \left(M^2 + \frac{1}{12} h^2 \Delta N^2 \right) \quad (9)$$

G represents strain energy release rate for circular blister propagation, M is bending moment and N is resultant stress force ($\sigma = \sigma_r - \sigma_d$) acting on coating. By incorporating the coupling effect of compressive residual stress and diffusion induced stress in crack propagation can be derived as:

$$G' = 6 \frac{(1-\nu^2)}{E h^3} M^2 \left(1 + \frac{1}{4} \left(\sqrt{\left(\frac{\partial \sigma_{r_c}}{\partial x} - \frac{\partial \sigma_{d_c}}{\partial t} \right)^2 \sigma_{cr}^{-1}} - 1 \right) \right) \quad (10)$$

The term $\left(\frac{\partial \sigma_{r_c}}{\partial x} - \frac{\partial \sigma_{d_c}}{\partial t} \right) \sigma_{cr}^{-1}$ is de-bonding index which controls blister formation and propagation. By using relation of mode dependent strain energy release rate the following model can be formulated for de-bonding driving force.

$$F = 6 \frac{(1-\nu^2)}{E h^3} M^2 \left(1 + \frac{1}{4} (\sqrt{\Gamma-1})^2 \right) \left(\sec^2 \left[\left(1 - \frac{\Gamma_{IC}}{E_c \lambda} \right) \psi \right] \right)^{-1} \quad (11)$$

F represents de-bonding driving force, Γ_{IC} is coating toughness, λ is roughness of substrate interface and ψ is the ratio of coating crack edge from mode II to mode I.

4.2 De-bonding driving force for straight-sided blister

The derivation of de-bonding driving force for straight-sided blister propagation is proposed and derived in this section. The straight-sided blister proliferates after the complete formation of curved ‘front’ of blister. The straight-sided blister is thought to provide accurate measure of primary area of de-bonded interface needed to initiate buckle delamination along with energy release rate [27]. The strain energy release rate [27] in direction parallel to crack front can be written as:

$$G_0 = \frac{(1-\nu^2)}{2 E} \sigma_0^2 h \quad (12)$$

By incorporating the $\sigma_0 = \frac{\partial \sigma_{r_c}}{\partial t} - \frac{\partial \sigma_{d_c}}{\partial t}$ stress, which has been concluded in previous section in the above equation, the strain energy release rate for straight-sided blister due to coupling effect of compressive residual stress and diffusion induced stress can derived as:

$$G'_0 = \frac{(1-\nu^2)h}{2 E} \left(\frac{\partial \sigma_{r_c}}{\partial t} - \frac{\partial \sigma_{d_c}}{\partial t} \right)^2 \quad (13)$$

In straight-sided blister, the energy release rate relation for crack propagation at ‘side’ and ‘front’ has separate relations [27]. The ‘side’ and ‘front’ sides of straight-sided blister is labelled in Fig. 3. For blister side strain energy as a function of stresses can be written as:

$$G_{side} = G_0 \left(1 - \frac{\sigma_c}{\sigma_0} \right) \left(1 + 3 \frac{\sigma_c}{\sigma_0} \right) \quad (14)$$

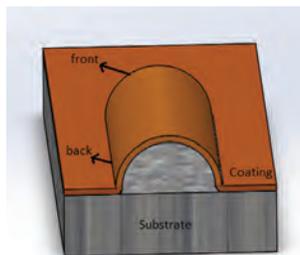


Figure 3: Schematic of straight-sided blister.

By incorporating the $\sigma_0 = \frac{\partial \sigma_{r_c}}{\partial t} - \frac{\partial \sigma_{d_c}}{\partial t}$ in the above relation the strain energy for 'side' of blister as a function of coupling effect of compressive residual stress and diffusion induced stress can be written as:

$$G'_{side} = \frac{(1-\nu^2)h}{2E} \left(\frac{\partial \sigma_{r_c}}{\partial t} - \frac{\partial \sigma_{d_c}}{\partial t} \right)^2 \left(1 - \sigma_c \left(\frac{\partial \sigma_{r_c}}{\partial t} - \frac{\partial \sigma_{d_c}}{\partial t} \right)^{-1} \right) \left(1 + 3\sigma_c \left(\frac{\partial \sigma_{r_c}}{\partial t} - \frac{\partial \sigma_{d_c}}{\partial t} \right)^{-1} \right). \quad (15)$$

De-bonding driving force for the 'side' of blister as a function of mode mix can be derived as:

$$F_{side} = \frac{(1-\nu^2)h}{2E} \sigma_0^2 (1 - \alpha_c^{-1}) (1 + 3\alpha_c^{-1}) \left(\sec^2 \left[\left(1 - \frac{\Gamma_{IC}}{E_c \lambda} \right) \Psi \right] \right)^{-1}. \quad (16)$$

F_{side} is the de-bonding driving force for 'side' of straight-sided blister, which is a function of mod mix and de-bonding index. Similarly, the de-bonding driving force for 'front' of blister can be derived as follows:

$$G_{front} = G_0 \left(1 - \frac{\sigma_c}{\sigma_0} \right). \quad (17)$$

By including de-bonding index in eqn (13), it can be modified as:

$$G'_{front} = \frac{(1-\nu^2)h}{2E} \left(\frac{\partial \sigma_{r_c}}{\partial t} - \frac{\partial \sigma_{d_c}}{\partial t} \right)^2 \left(1 - \sigma_c \left(\frac{\partial \sigma_{r_c}}{\partial t} - \frac{\partial \sigma_{d_c}}{\partial t} \right)^{-1} \right). \quad (18)$$

De-bonding driving force for the 'front' of blister as a function of mode mix can be derived as:

$$F_{front} = \frac{(1-\nu^2)h}{2E} \sigma_0^2 (1 - \alpha_c^{-1}) \left(\sec^2 \left[\left(1 - \frac{\Gamma_{IC}}{E_c \lambda} \right) \Psi \right] \right)^{-1}. \quad (19)$$

The 'front' and 'side' de-bonding driving forces for straight-sided blister are proposed by incorporating the coupling effect of compressive residual stress and diffusion induced stress.

5 SIMULATION RESULTS

5.1 Simulation results for circular blister

The resultant stress force due to coupling effect of compressive residual stress and diffusion induced stress proposed for circular blister formation and propagation has been validated which shows strong agreement between experimental observation and mathematical modelling [16]. Experimental and simulation results for normalised de-bonding driving force as a function of change in temperature are shown in Fig. 4. All parameters are converted into dimensionless form for simulation of normalised de-bonding driving force. In region 1, the coating and substrate system was in safe condition and there was no change in pre-existing micro-crack and de-bonding driving force was also zero. In region 2, micro-crack

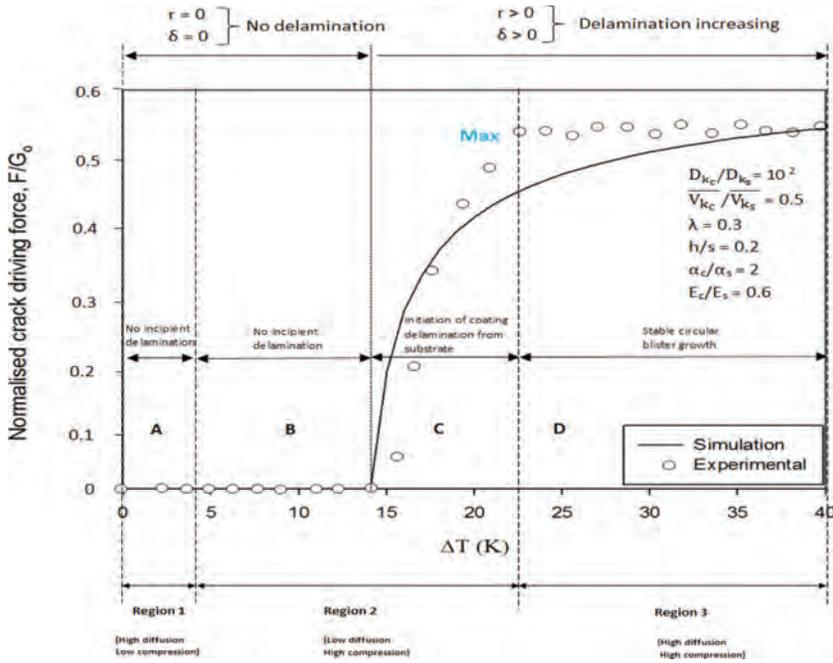


Figure 4: Simulation and experimental results of de-bonding driving force for circular blister [16].

aperture size started to reduce due to high compression rate. Diffusion rate decreased due to the reduction in aperture size of micro-crack. Normalised de-bonding driving force was zero till $\Delta T = 14\text{K}$; hence, coating can be considered in safe condition. Further increase in temperature resulted in adhesion loss in the form of blistering and de-bonding driving force continued to increase and reach at maximum level. In region 3, compressive residual stress continues to increase and the behaviour of diffusion rate seems similar to compressive residual stress. In this region the size of blister increased significantly and micro-crack also expanded.

5.2 Simulation results for straight-sided blister

The proposed mathematical models for straight-sided blister is based on validated theory as explained in previous sections [16, 27]. The simulation result of straight-sided blister is shown in Fig. 5. The mathematical equations for simulating de-bonding driving forces for ‘side’ and ‘front’ were converted into normalised form. It is worth noting that the de-bonding driving force for the ‘side’ of straight-sided blister is always greater as compared to the de-bonding driving force for the ‘front’ but crack propagates at the ‘front’. The reason is that the ‘front’ experiences lower effective interface toughness [27]. For sufficiently wide straight-sided blister, the energy release rate along curved front exceeds than that of ‘side’ for large (by a factor of ten or more) coating modulus than substrate which would allow propagation of straight-sided blisters despite of interface toughness is mode independent [28].

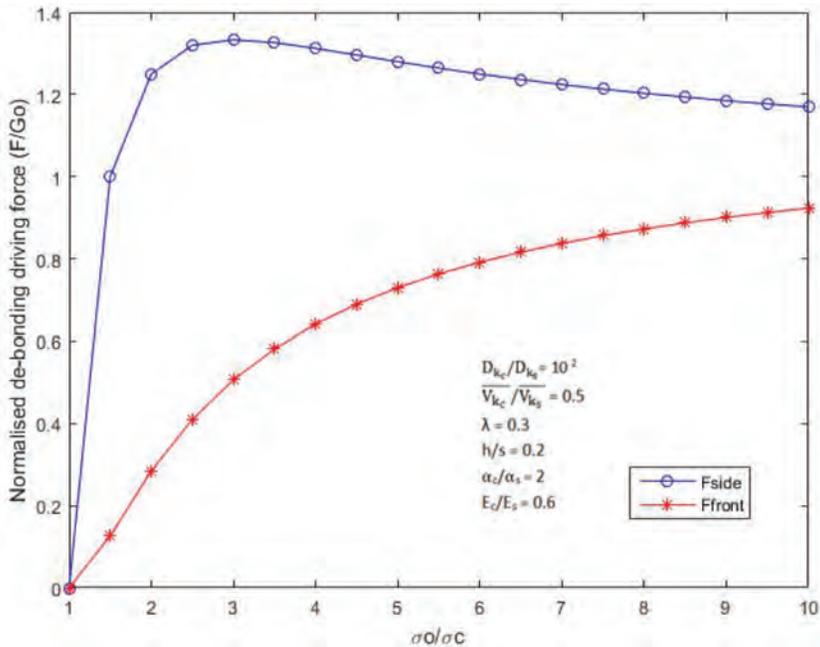


Figure 5: Simulation results of de-bonding driving forces for straight-sided blister.

6 CONCLUSIONS

This paper presents the mathematical modelling for circular and straight-sided blister growth and propagation by incorporating coupling effect of compressive residual stress and diffusion induced stress. The effects of stresses are investigated in the presence of micro-cracks. The difference in coefficient of thermal expansion between coating and substrate system induced compressive residual stress which continued to increase due to an increase in temperature while the corrosive species produced diffusion induced stress. Initially, increase in temperature caused pre-existing micro-crack to shrink and reduce diffusion induced stress while further increase in temperature caused de-bonding driving force to exceed its critical level which resulted in blister formation and it started propagating in circular shape. The rising trend of diffusion induced stress appears to be similar as compressive residual stress at high temperature. Based on experimental observations, resultant stress for blister formation and growth is proposed and incorporated in circular and straight-sided blisters formation and propagation to propose the de-bonding driving forces. De-bonding driving forces are proposed for blisters growth and propagation which can be used for coating life assessment. Proposed mathematical models can be further extended for ‘telephonic cord’ which appears after the propagation of circular blister and for ‘back and forth’ shape which appears after the propagation of straight-sided blister. Comprehensive analyses of circular blister formation and propagation has been conducted through experimentation and by simulating the effects of various parameters (modulus of elasticity, coefficient of thermal expansion, coating thickness and poisson’s ration) in previous NCEM papers. In future, further analysis of proposed de-bonding driving forces of straight-sided blisters will be presented.

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